

### Abstract

A novel method is presented to measure inductor losses – based on an actual power conversion application.

Compared to commercial lab equipment, hard switching of the inductor is used to provide information about:

- AC loss
- DC loss
- Dynamic saturation
- Self heating prediction

This patented measurement method was implemented in a commercially available measurement system for discrete inductors, MADMIX.

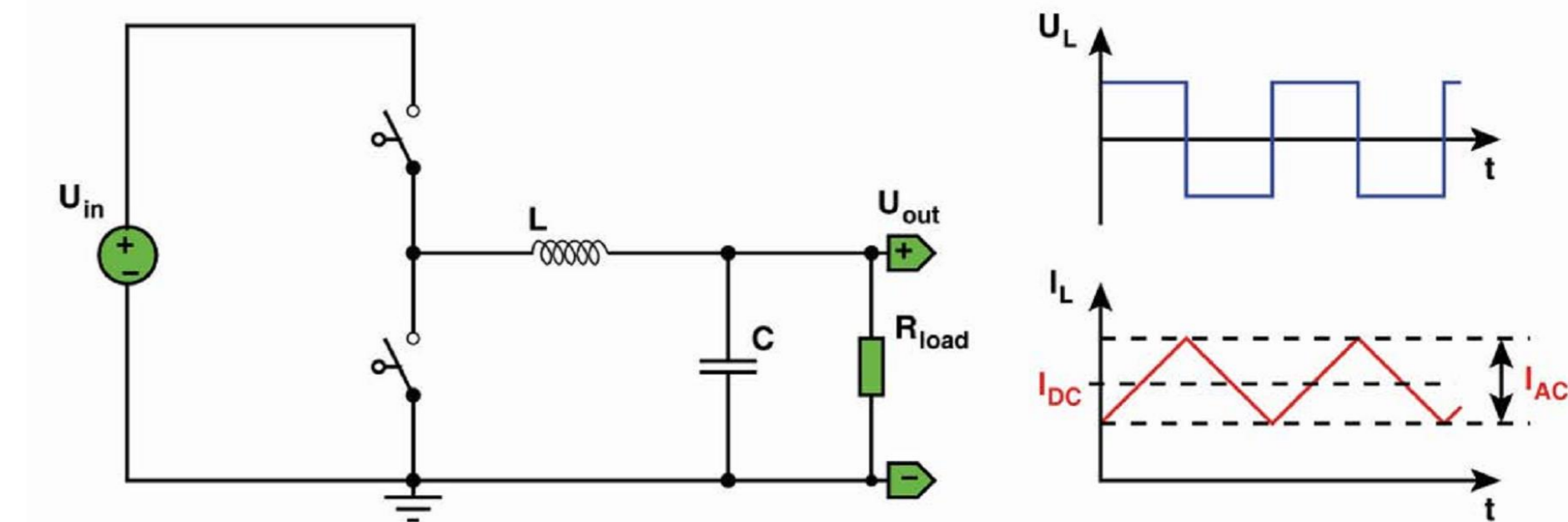
The described measurement method was proven using a custom developed high-speed driver with small footprint air-core and ferrite inductors, as a proof-of-concept for the measurement of fully-integrated inductors.

### Objective

- High-speed and highly/fully integrated inductive convertors require a careful trade-off between the involved power losses in the power switches, and power inductor, to maintain converter efficiency.
- While fairly straightforward to assess the driver losses, it has become critical to understand saturation and loss dynamics involved in the power inductor.
- Existing methods for measuring inductors and their losses depend on small signal analysis, not representative for the switching application
- **Objective** : provide a method for measuring inductor losses, saturation effects and inductance variations depending on the operating point, suitable for integrated inductors.

### Method

The inductor-under-test is hard switched, while measuring the transient inductor voltage and currents.



By post-processing of the transient inductor and current waveforms, the inductance, the AC and DC power loss and dynamic saturation can be calculated [3]:

$$L = \frac{R_{LS} \cdot t_{on}}{\ln \left[ \frac{I_{min} \cdot R_{LS} - U_{Lg1}}{I_{max} \cdot R_{LS} - U_{Lg1}} \right]}$$

$$P_{loss} = \frac{1}{T} \cdot \int_0^T i_L(t) \cdot u_L(t) dt$$

### Measurements

The described measurement method was proven using a custom developed high-speed driver with small footprint air-core inductors, as a proof-of-concept for the measurement of fully-integrated inductors.

2 inductors were compared to quantify total  $P_{AC}$  over a frequency range of 6 – 20 MHz.

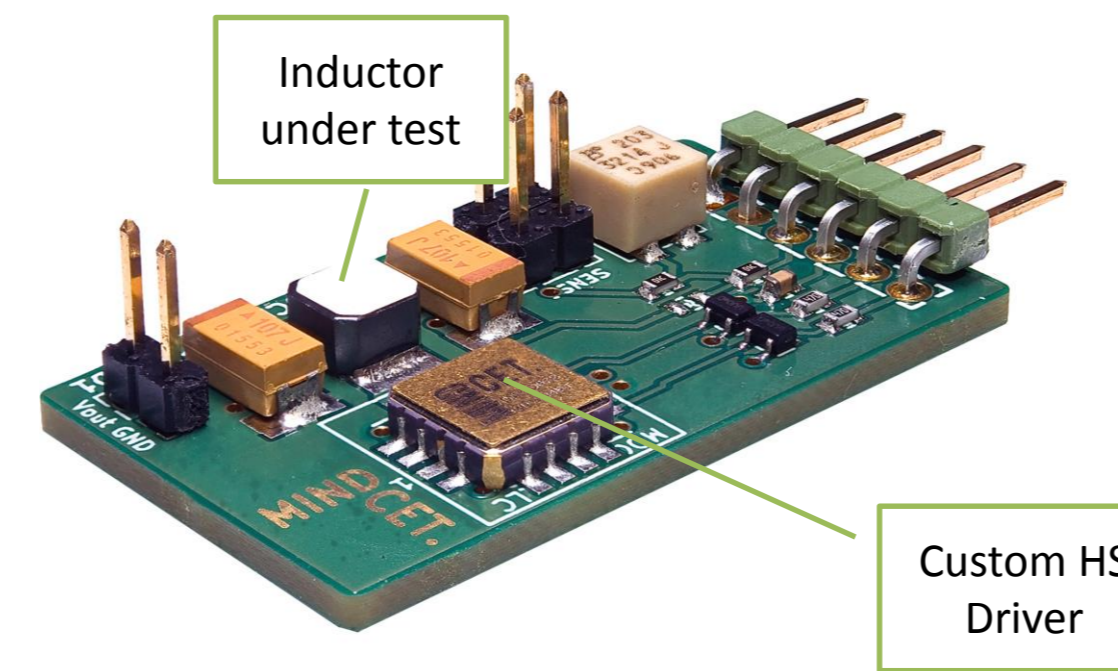
#### Inductor A :

- 150nH aircore inductor, with RDC = 590mOhm

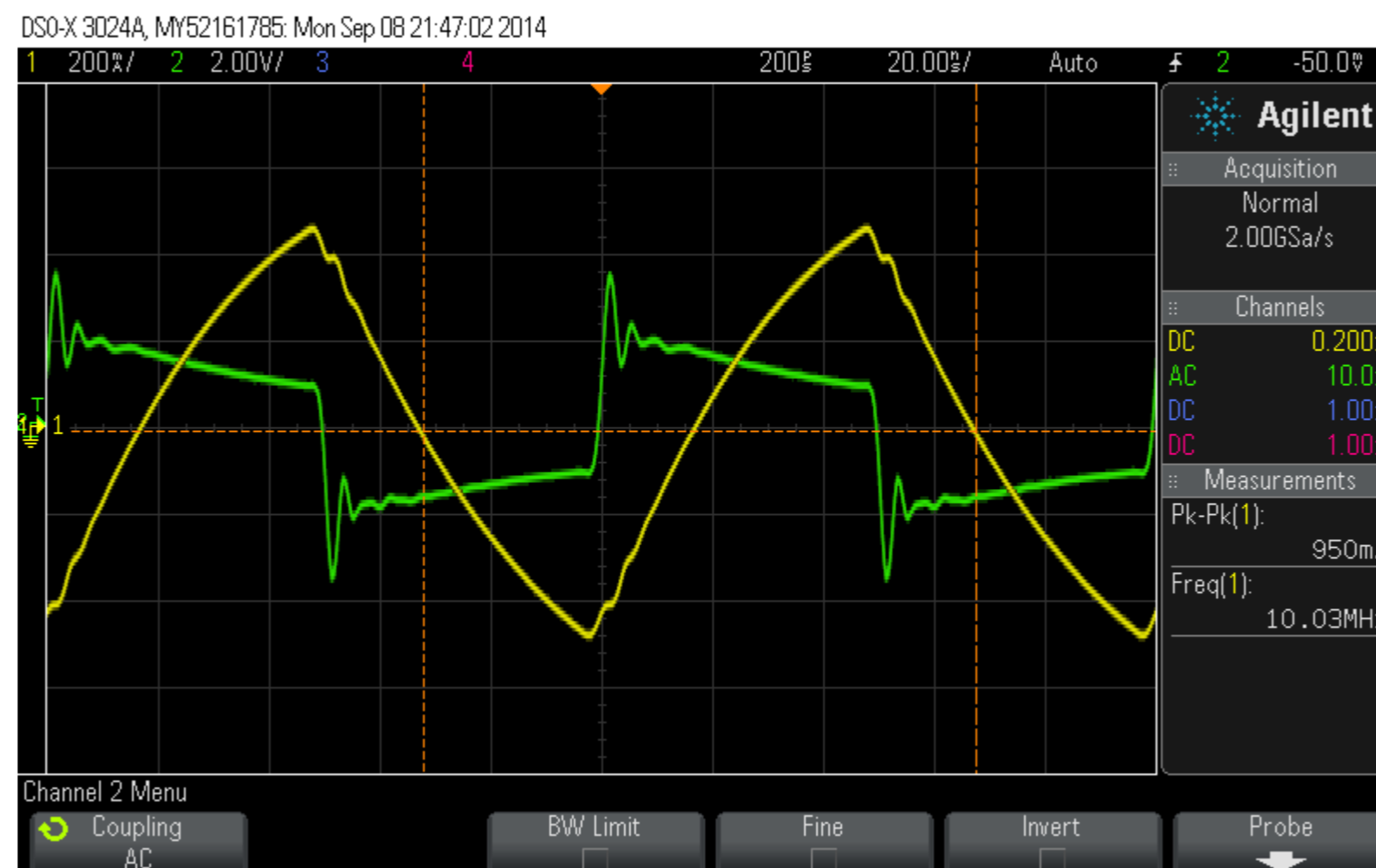
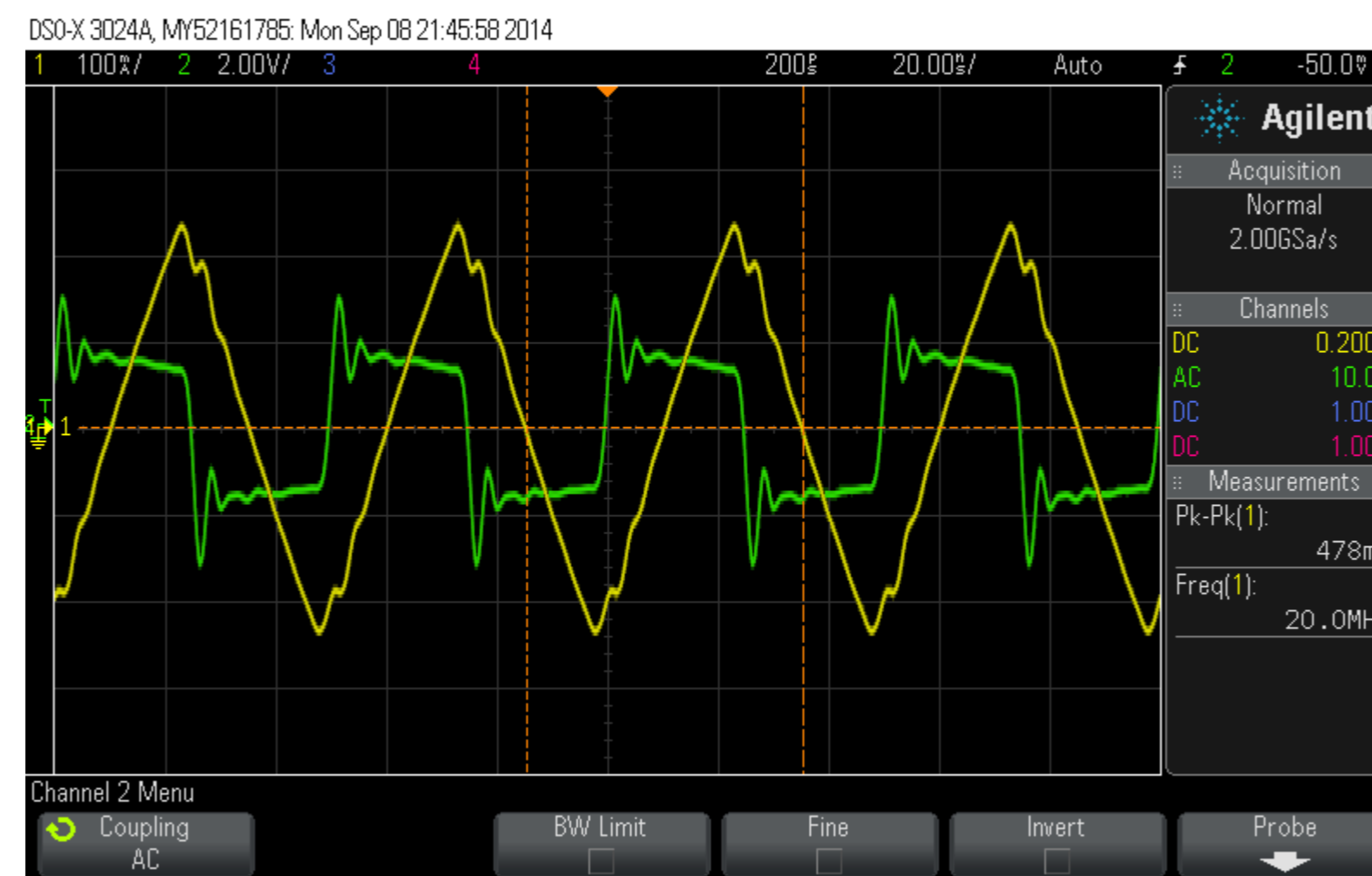
#### Inductor B:

- 180 nH ferrite inductor, with RDC = 1.6mOhm

### Measurement setup

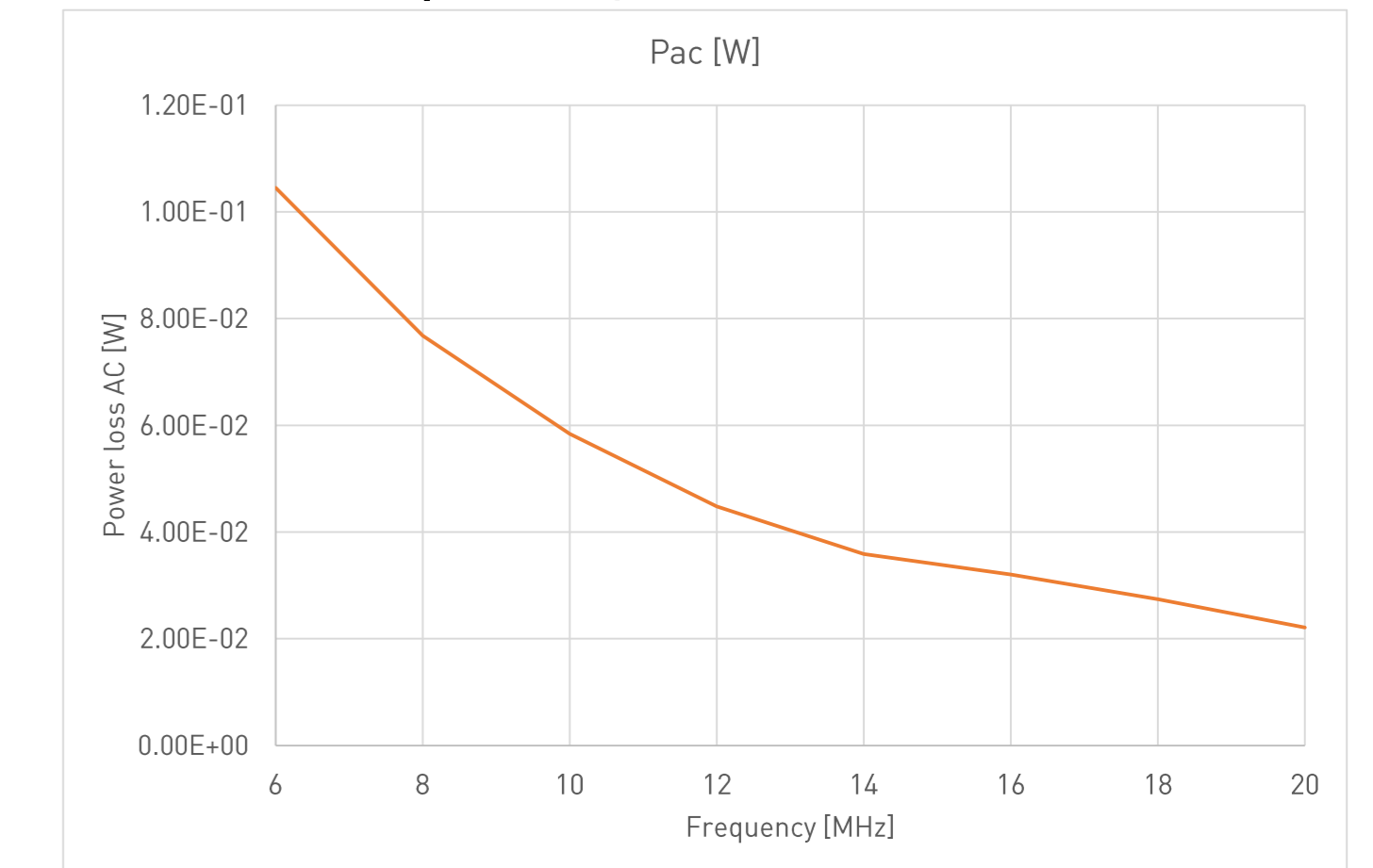


### Inductor V/I waveforms



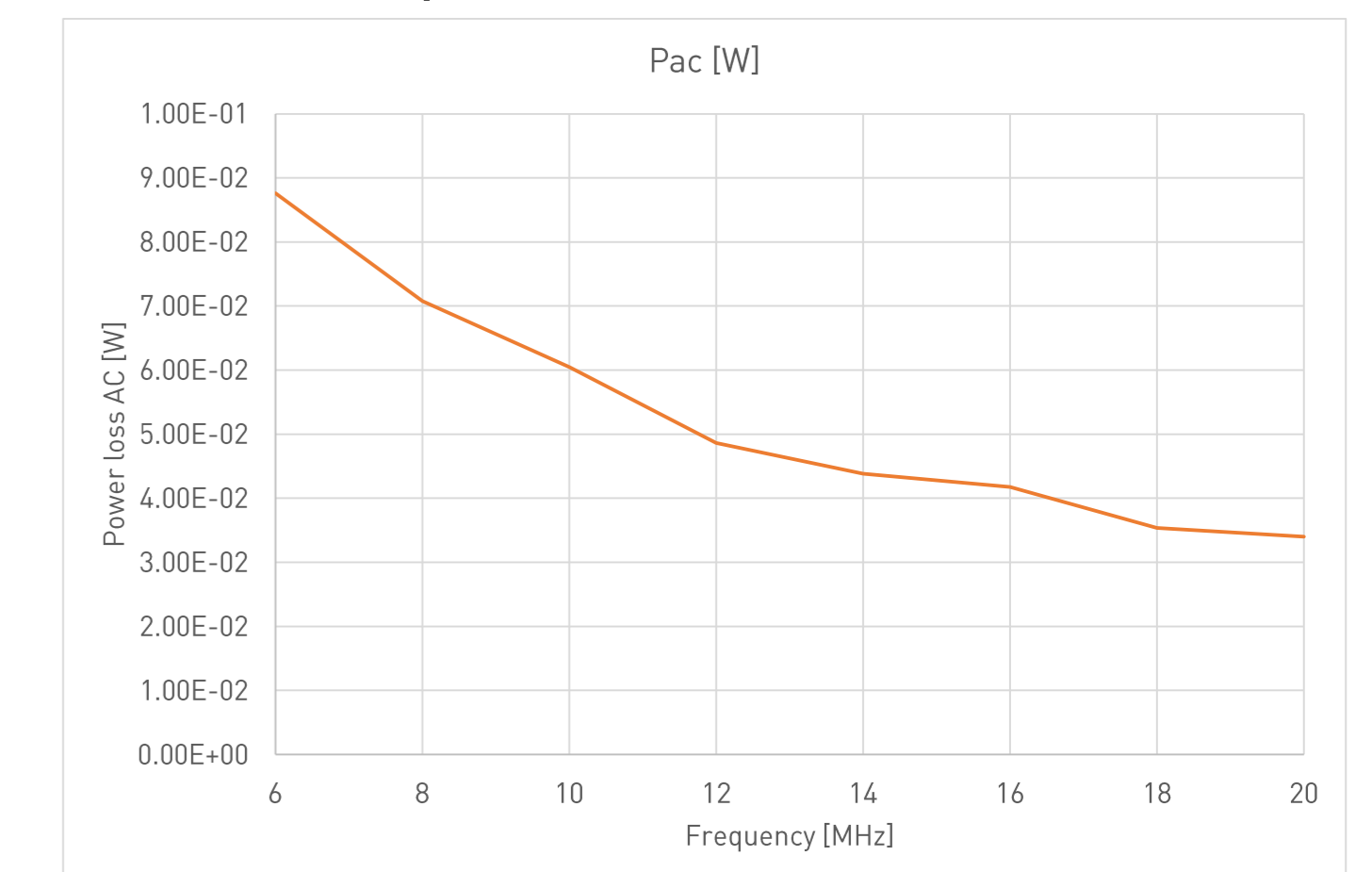
### Inductor A

#### AC losses vs frequency



### Inductor B

#### AC losses vs frequency



### Interpretation

For a given inductance, the ripple current decreases with an increasing switching frequency.

#### Inductor A (aircore)

- AC Power losses are determined by the total resistance (DC resistance and skin effect) and the RMS current.

#### Inductor B (ferrite core)

- AC Power losses are determined by the ferrite core losses, which depend largely on the current ripple magnitude.

### Conclusion

Conventional inductor loss measurement use small signal impedance analysis, at sinewave excitation [1] or core loss estimation through B-H curve measurement [2]. These methods do not reflect the actual power conversion application with hard-switched waveforms.

The proposed method provides the power designer the proper data to maximally optimize its converter design: inductor power loss, inductance, dynamic saturation, self-heating prediction, ... at any given operating point.

### References

- [1]<http://cp.literature.agilent.com/litweb/pdf/5950-2367.pdf>
- [2][https://www.iti.iwatsu.co.jp/en/products/sy/bh\\_ana\\_e.html](https://www.iti.iwatsu.co.jp/en/products/sy/bh_ana_e.html)
- [3]<http://worldwide.espacenet.com/publicationDetails/biblio?CC=W0&NR=2013110145A1&KC=A1&FT=D>