



***Potential Benefits of Integrated
Switching Power Converters:
Inductive vs. Switched-Capacitor***

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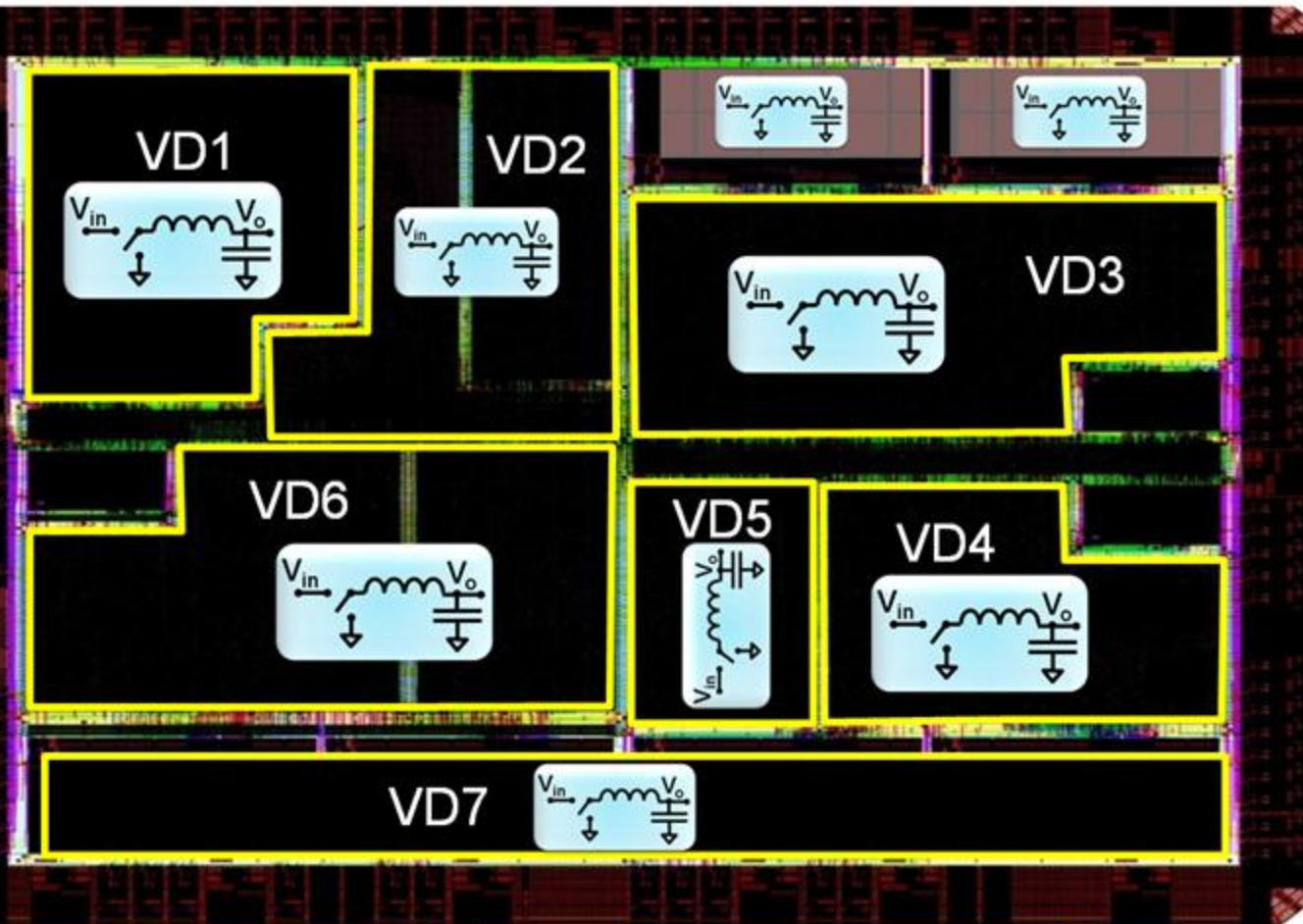
Outline

- ▶ Introduction: distributed power systems
- ▶ State of the art
- ▶ Scalability of inductive power converters
- ▶ Scalability of switched-capacitor power converters
- ▶ Multiphase designs
- ▶ Conclusions

Introduction

Introduction: Power distributed systems

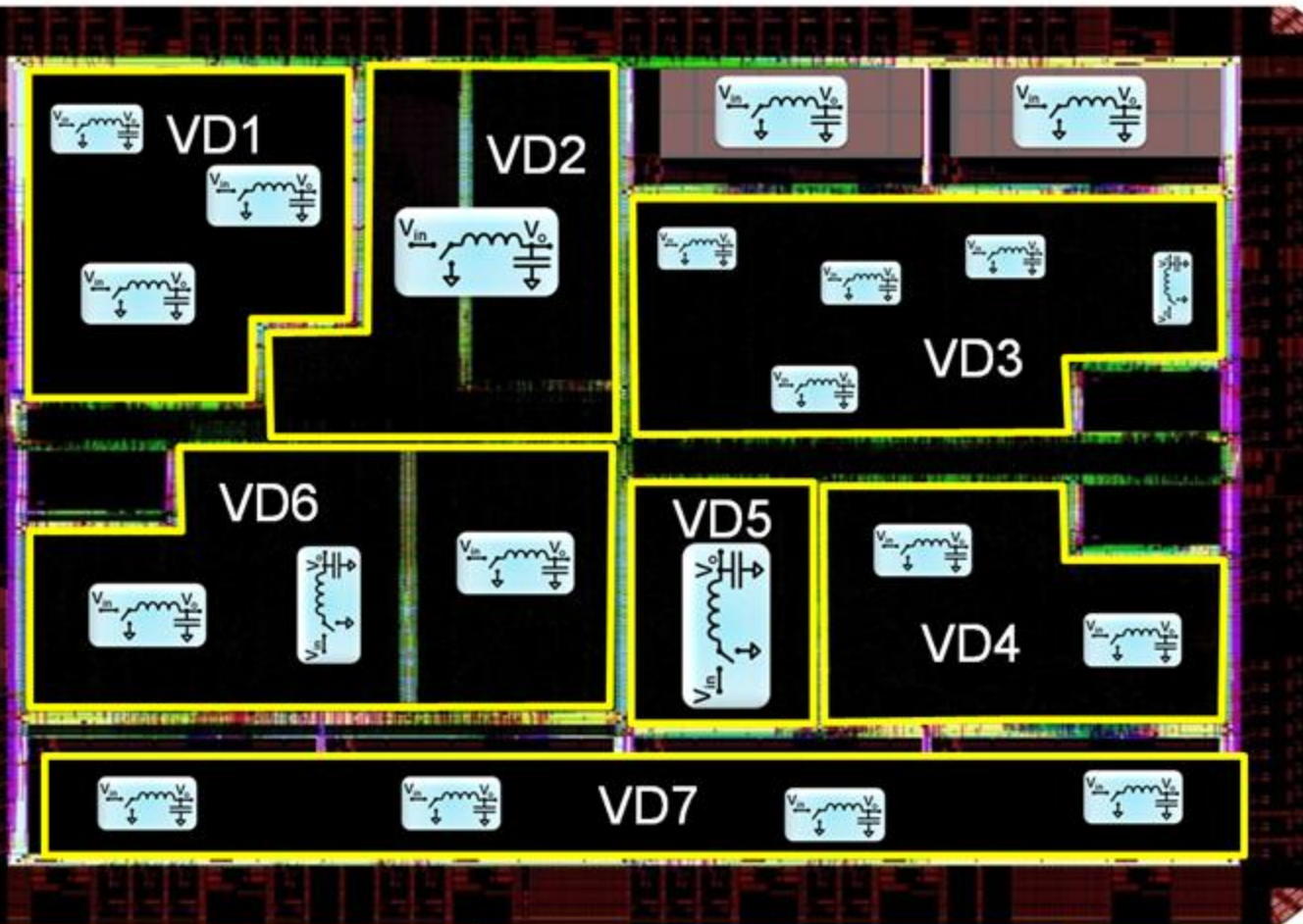
Case 1: One converter per voltage domain



- Efficient generation of different voltage domains
- Adaptability to different specs per block
- Low power converters

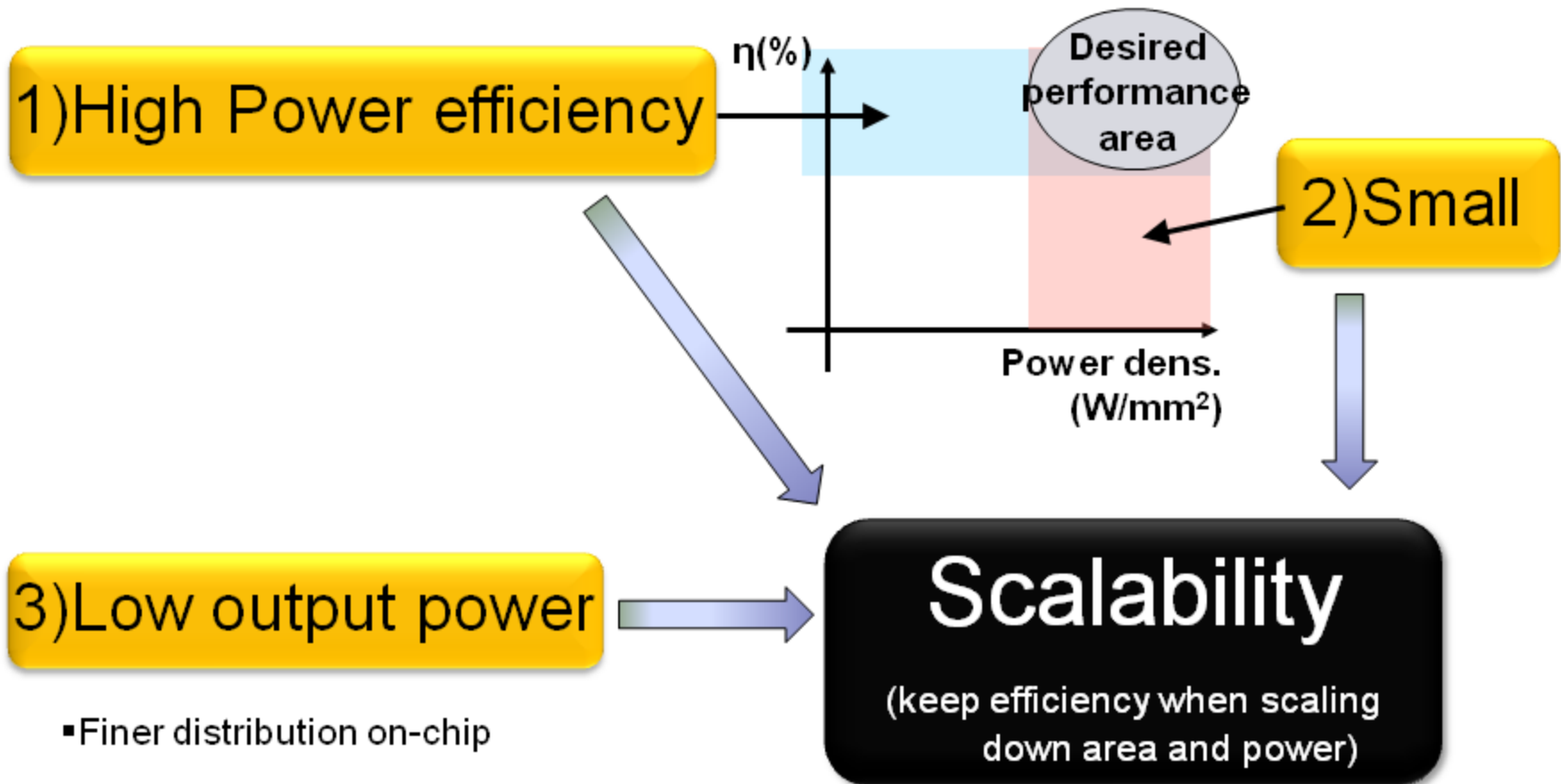
Introduction: Power distributed systems

Case 2: Multiple converters per voltage domain



- Efficient generation of different voltage domains
- Adaptability to different specs per block
- Local regulation
 - Better power distribution
 - Even lower power per converter

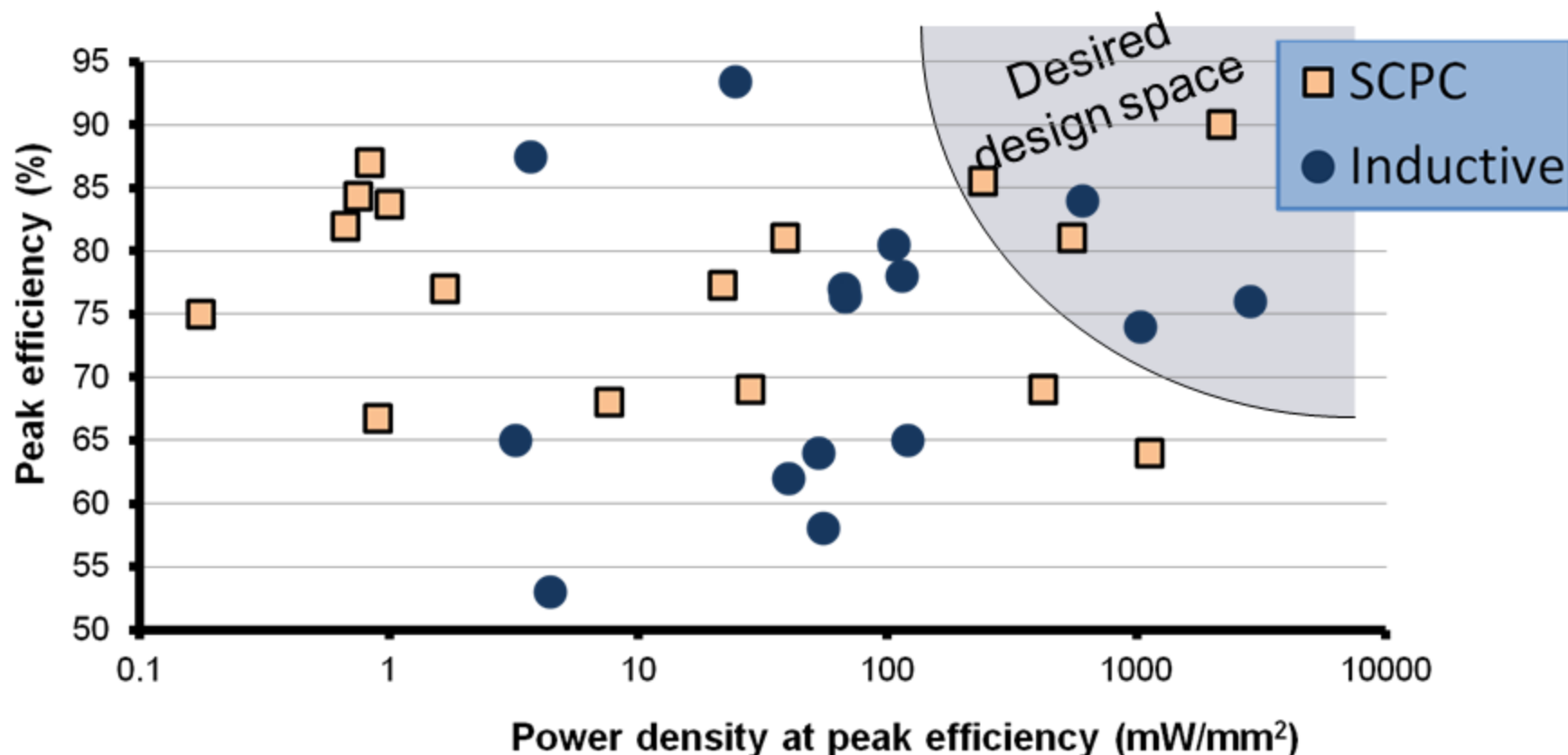
Requirements





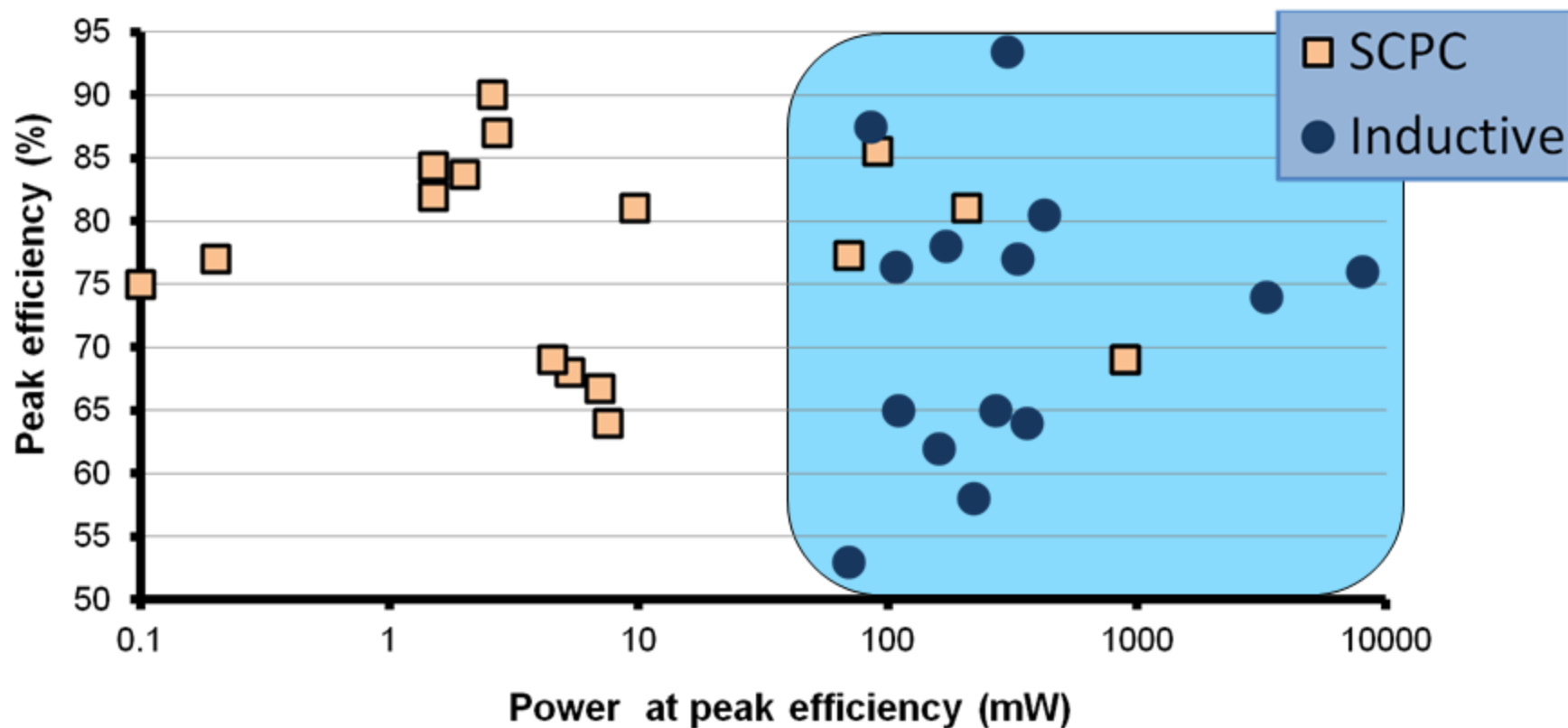
State of the art

State of the art: fully integrated converters



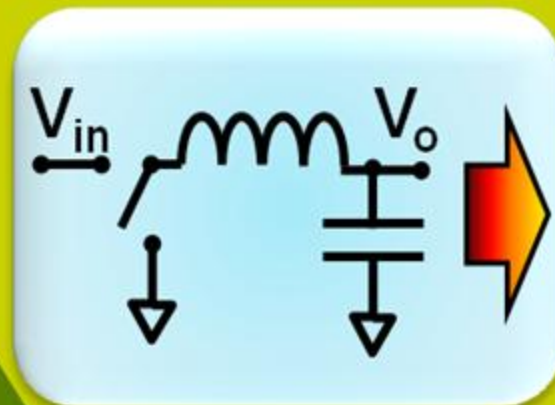
No clear advantage in performance

State of the art: fully integrated converters

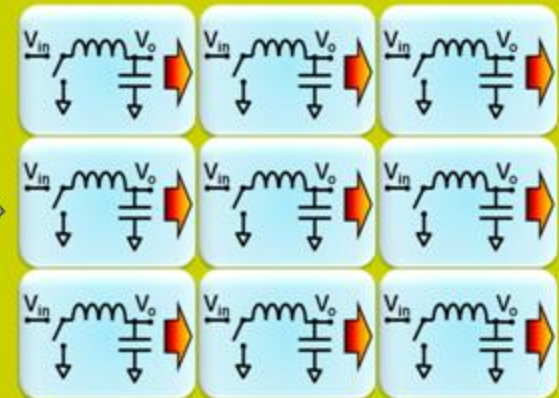


Inductive designs always focus on high power

Scalability of inductive converters



x modules



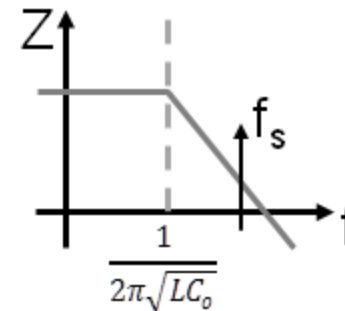
Scalability of inductive converters (I)

Split the converter into 'x' modules:

- Scale size of L & C_o to keep constant ΔV_o at constant f_s :

$$-C_o \rightarrow C_o/x$$

$$-L \rightarrow x^*L \text{ (reduce area but increase inductance)}$$



- Inductor current RMS for CCM buck converter:

$$I_L^2 = I_o^2 + \frac{V_o^2 (V_{in} - V_o)^2}{12V_{in}^2 f_s^2 L^2} \xrightarrow{I_o \rightarrow \frac{I_o}{x}; L \rightarrow xL} I_L^2 \sim \frac{1}{x^2} \rightarrow \text{Also applies to DCM}$$

- The switches should also be scaled:

$$\bullet R_{on} \rightarrow x^*R_{on}; I_{NMOS} \text{ \& } I_{PMOS} \text{ RMS reduces by } x^2 \rightarrow P_{NMOS,PMOS} \sim \frac{1}{x}$$

$$\bullet \text{Switching losses should also reduce with the size of the components (keeping } f_s \text{ constant)} \rightarrow P_{sw} \sim \frac{1}{x}$$

Scalability of inductive converters (II)

Efficiency: $\eta = \frac{P_o}{P_o + P_L + P_{N,P} + P_{sw}}$

▪ Inductor conduction losses:

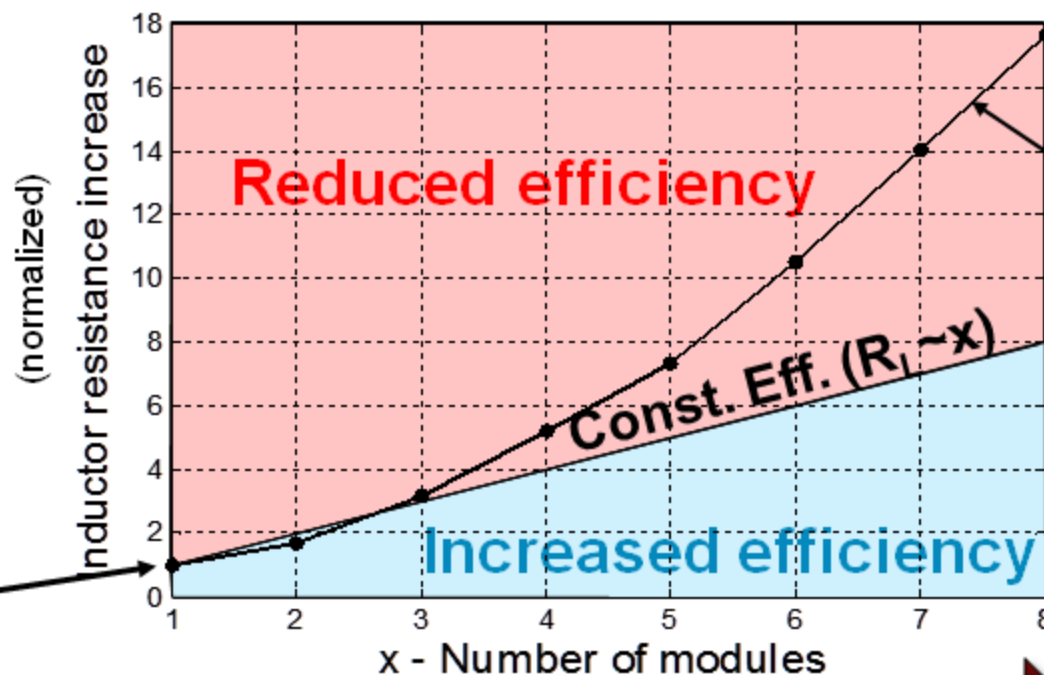
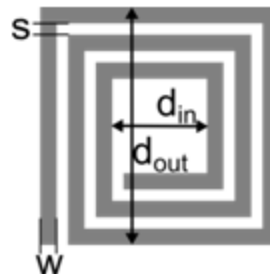
$$P_L \sim \frac{1}{x} \xrightarrow{\begin{matrix} P_L = I_L^2 R_L \\ I_L^2 \sim \frac{1}{x^2} \end{matrix}} R_L \sim x$$

To keep a constant efficiency, the inductor resistance should be proportional to the number of modules (x), so that the inductor losses reduce with the same factor.

Scalability of inductive converters (III)

- Example with planar spiral inductors:

$$L = \frac{K_1 \mu N_L^2 d_{avg}}{1 + K_2 \rho}$$

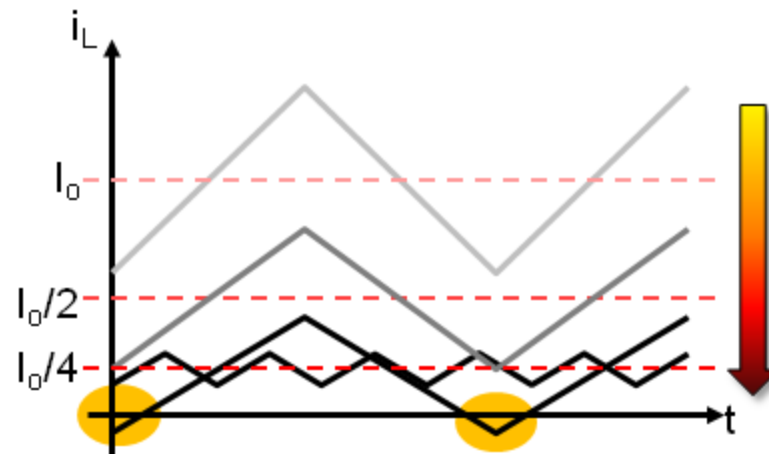


Area reduces & Inductance increases

Scalability of inductive converters (III)

Efficiency of inductive converters
will drop when scaling down
output power and size

Inductive converters moving to DCM...



Increasing number of modules (x):

- Reduces I_o (per modules) $\rightarrow I_o/x$
- Increases L , **but not** $\rightarrow x \cdot L$!!

Increasing switching frequency
reduces current ripple at the cost of
switching losses increase

High number of modules

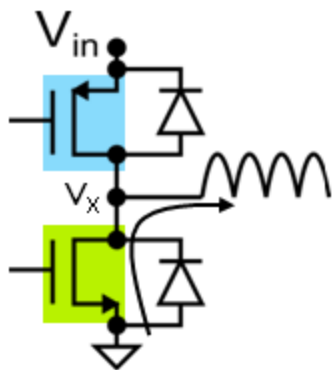
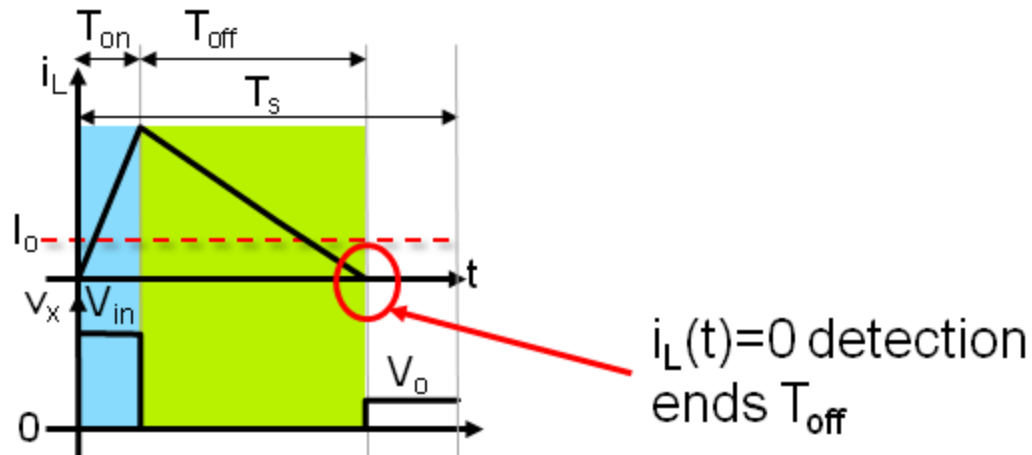
Discontinuous Conduction Mode

- High RMS value $i_L(t) \rightarrow P_{\text{cond}} \uparrow$
- Zero-current switching $\rightarrow P_{\text{sw}} \downarrow$

Edge DCM \leftrightarrow CCM

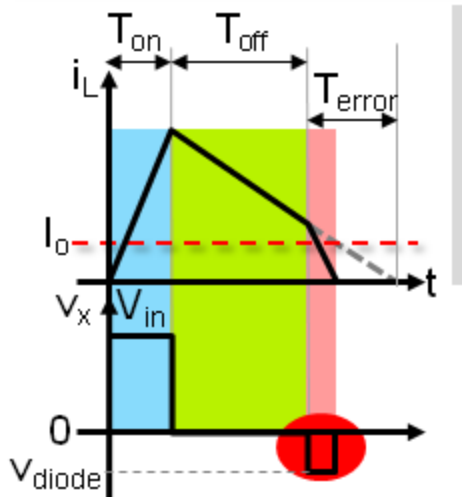
Inductor current zero-crossing detection:

Right T_{off} phase duration:

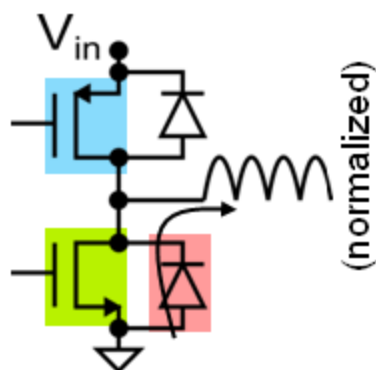


Inductor current zero-crossing detection:

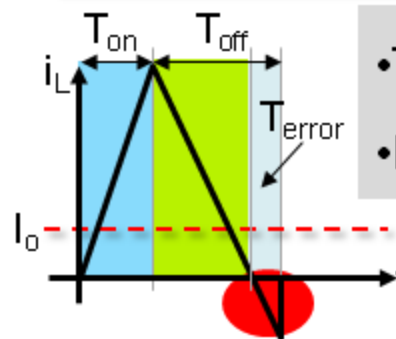
Too short T_{off} phase:



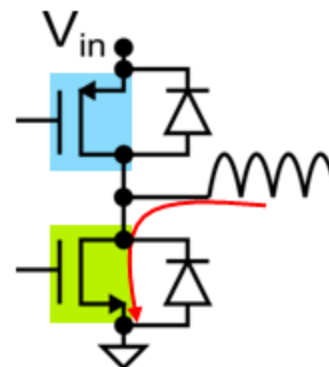
- $T_{\text{on}} \uparrow \rightarrow I_{\text{LRMS}} \uparrow \rightarrow P_{\text{cond}} \uparrow$
- $I_{\text{Lmax}} \uparrow \rightarrow P_{\text{sw}} \uparrow$
- $i_L * V_{\text{diode}} \rightarrow P_{\text{cond}} \uparrow$



Too long T_{off} phase:

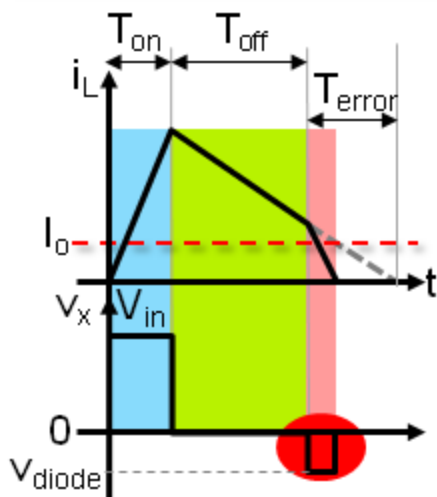


- $T_{\text{on}} \uparrow \rightarrow I_{\text{LRMS}} \uparrow \rightarrow P_{\text{cond}} \uparrow$
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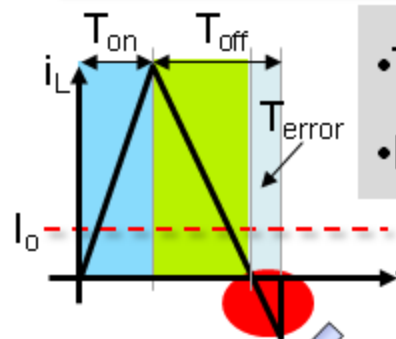
Inductor current zero-crossing detection:

Too short T_{off} phase:



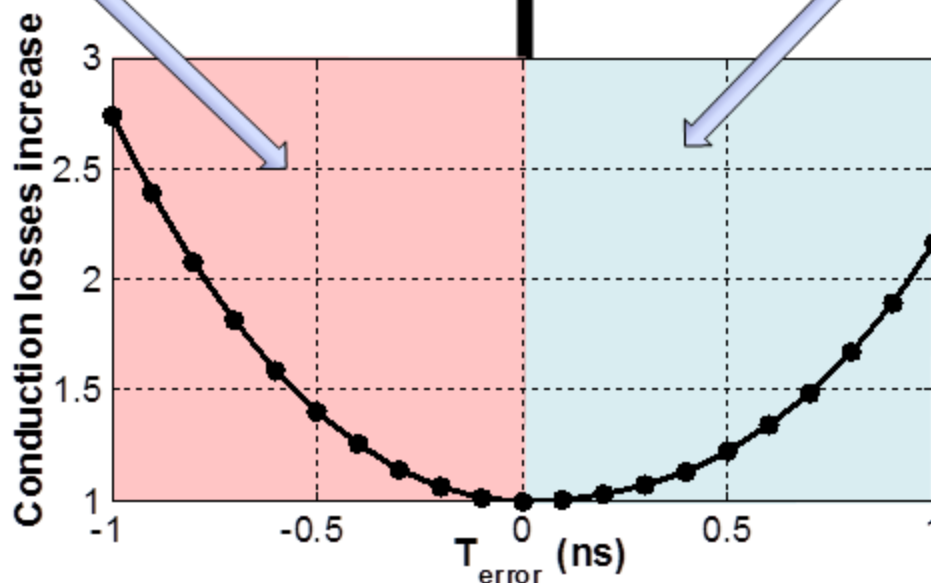
- $T_{on} \uparrow \rightarrow I_{LRMS} \uparrow \rightarrow P_{cond} \uparrow$
- $I_{Lmax} \uparrow \rightarrow P_{sw} \uparrow$
- $i_L * V_{diode} \rightarrow P_{cond} \uparrow$

Too long T_{off} phase:



- $T_{on} \uparrow \rightarrow I_{LRMS} \uparrow \rightarrow P_{cond} \uparrow$
- $I_{Lmax} \uparrow \rightarrow P_{sw} \uparrow$

(normalized)

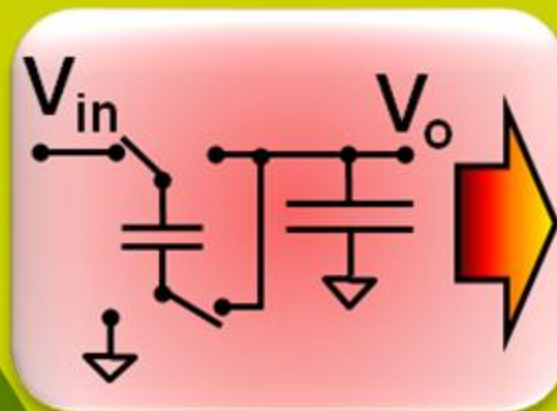


- $V_{in}=1.8V$
 - $V_o=1V$
 - $I_o=100mA$
 - $L=2nH$
 - $C_o=7.5nF$
 - $f_s=175MHz$
 - $\Delta V_o=5\%$
 - $R_{on}=0.1\Omega$; $R_L=0.38\Omega$
 - $V_{diode}=0.7V$
- 1mm²

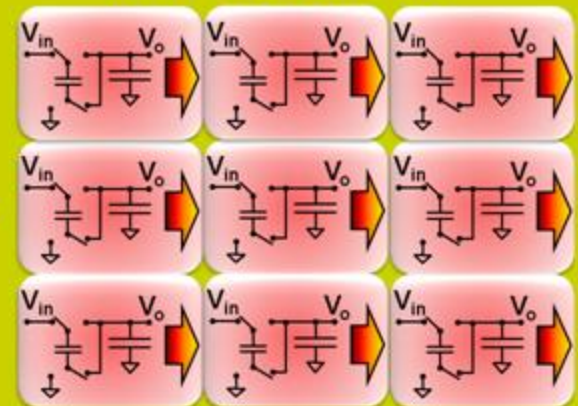
Inductor current zero-crossing detection:

Very few dedicated $i_L=0$ detection circuits
found for fully integrated inductive
converters

Scalability of switched-capacitor converters



x modules

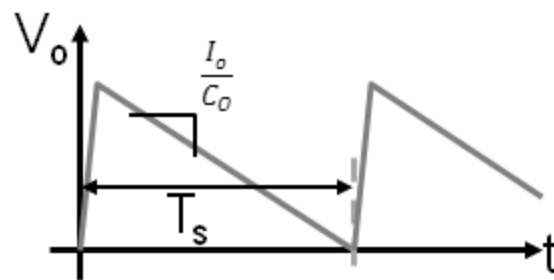


Scalability of switched-capacitor converters (I)

Split the converter into 'x' modules:

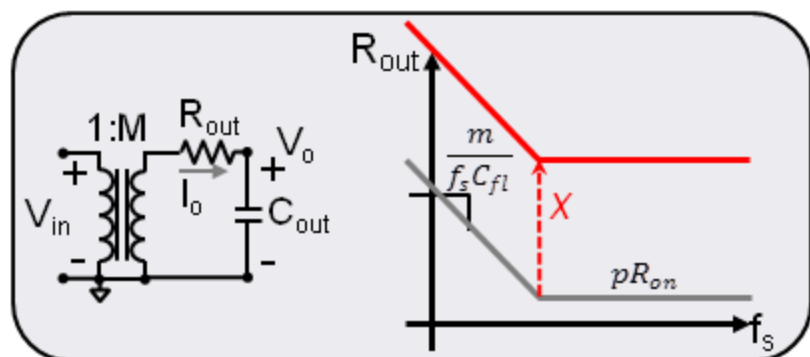
- Scale size of C_o to keep constant ΔV_o at constant f_s :

$$\Delta V_o = \frac{I_o}{f_s C_o} \xrightarrow{I_o \rightarrow \frac{I_o}{x}; C_o \rightarrow \frac{C_o}{x}} \Delta V_o = ct.$$



- Output impedance:

$$R_{out} = \sqrt{\left(\frac{m}{f_s C_{fl}}\right)^2 + (pR_{on})^2} \xrightarrow{R_{on} \rightarrow xR_{on}; C_{fl} \rightarrow \frac{C_{fl}}{x}} R_{out} \sim x$$



- Output power:

$$P_o = MV_{in} I_o - I_o^2 R_{out} \xrightarrow{I_o \rightarrow \frac{I_o}{x}; R_{out} \rightarrow xR_{out}} P_o \sim \frac{1}{x}$$

Scalability of switched-capacitor converters (II)

- Conduction losses:

$$P_{cond} = I_o^2 R_{out} \xrightarrow{I_o \rightarrow \frac{I_o}{x}; R_{out} \rightarrow x R_{out}} P_{cond} \sim \frac{1}{x}$$

- 'Bottom-plate' losses:

$$P_{bot} = f_s V_{in}^2 C_{bot} \xrightarrow{C_{bot} \rightarrow \frac{C_{bot}}{x}} P_{bot} \sim \frac{1}{x}$$

▪ Since switches become smaller driving switching losses will also scale down: $\rightarrow P_{sw} \sim \frac{1}{x}$

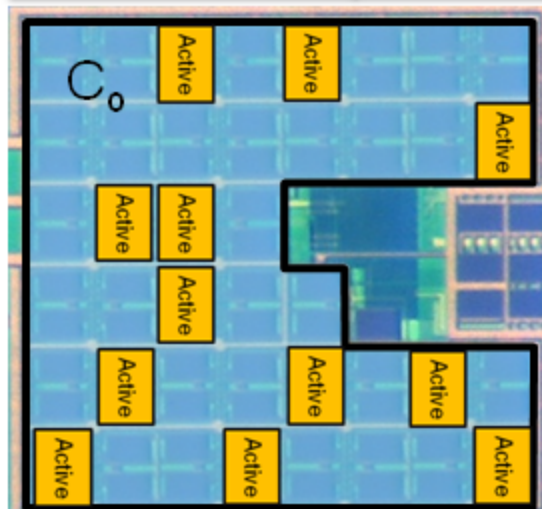
Efficiency of switched-capacitor converters will remain constant when scaling output power and size

$$\eta = \frac{P_o}{P_o + P_{cond} + P_{bot} + P_{sw}}$$

Multiphase designs

Multiphase has been applied to inductive & SC

Switched-capacitor:

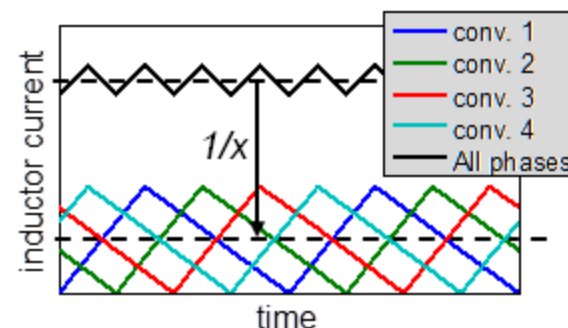
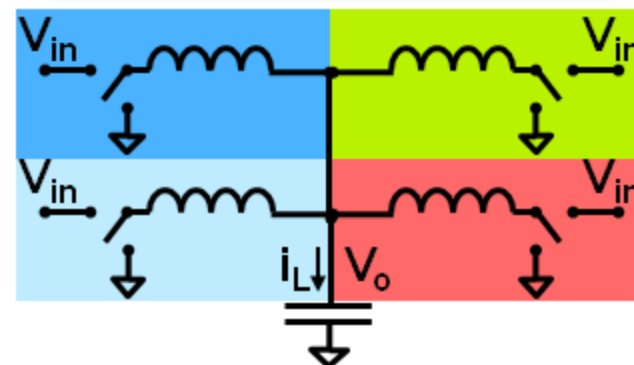


41 modules → Each module^{*1}:

- $I_o = 200 \mu A$
- $V_{in} = 1.6V$
- $V_o = 0.7V$
- $\eta = 78\%$
- $0.004 mm^2$

$$C_o = C_T - \frac{C_T}{x} \rightarrow \Delta V_o = \frac{I_o}{f_s C_T (x - 1)}$$

Inductive:



▪ Effective $i_L \rightarrow X$ times higher frequency

→ X times lower amplitude

$$\Delta V_o \sim \frac{1}{x^2}$$

^{*1} Gerard Villar Piqué; ISSCC'12

Multiphase has been applied to inductive & SC

Output capacitance is also determined by the required output impedance

Only applicable to power distribution case 2
(shared output node)

Conclusions

Conclusions

- ▶ No clear advantage for either kind of converter in terms of efficiency vs. power density.
- ▶ All the reported integrated inductive converters concentrate in the high range of output power.
- ▶ Inductive converters don't scale size and output power as well as switched capacitor converters.
- ▶ Switched-capacitor power converters look more promising for distributed power supplies.
- ▶ Multiphase approach improves the performance of both kind of converters but it can not always be applied.

Thank You!

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